

Universal optical amplification without nonlinearity

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We propose and experimentally realize a new scheme for universal phase-insensitive optical amplification. The presented scheme relies only on linear optics and homodyne detection, thus circumventing the need for nonlinear interaction between a pump field and the signal field. The amplifier demonstrates near optimal quantum noise limited performance for a wide range of amplification factors.

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Optical amplification is inevitably affected by fundamental quantum noise no matter whether it is phase sensitive or phase insensitive as stressed by Louisell *et al.* [1] and by Haus and Mullen [2]. The ultimate limits imposed by quantum mechanics on amplifiers was later concisely formulated by Caves [3] in fundamental theorems. This intrinsic noise, intimately linked with measurement theory and the no-cloning theorem, gives rise to many inextricable restrictions on the manipulations of quantum states. For example, microscopic quantum objects cannot be perfectly transformed, through amplification, into macroscopic objects for detailed inspection [4]: for phase insensitive amplification nonclassical features of quantum states, such as squeezing or oscillations in phase space, will be gradually washed out, and the signal to noise ratio of an information carrying quantum state will be reduced during the course of amplification. Despite these limitations, the universal phase insensitive amplifier is however rich of applications, in particular in optical communication. Amplifiers operating at the quantum noise limit are of particular importance for quantum communication where information is encoded in fragile quantum states, thus extremely vulnerable to noise.

Numerous apparatuses accomplish, in principle, ideal phase insensitive amplification as, for instance, solid state laser amplifiers [5], parametric downconverters [6] and schemes based on four wave mixing processes [7]. However, to date phase-insensitive amplification at the quantum limit has been only partially demonstrated [8, 9]: a number of difficulties are indeed involved in practice, especially for low gain applications. These difficulties mainly lie in the fact that the amplified field has to be efficiently coupled, mediated by a non linearity, to a pump field.

Following a recent trend in quantum information science, where non linear media are efficiently replaced by linear optics [10], we show in this Letter that universal phase insensitive amplification can also be achieved using only linear optics and homodyne detection. The simplicity and the robustness of this original scheme enable us

to achieve near quantum noise limited amplification of coherent states, even in the low gain regime.

Let us first briefly summarize the basic formalism describing a phase-insensitive amplifier [3]. Because of the symmetry of such an amplifier, it can be described by the following input-output transformation: $\hat{a}_{out} = \sqrt{G}\hat{a}_{in} + \hat{N}$ where $\hat{a}_{in(out)}$ represent the input (output) annihilation bosonic operators, G is the power gain and \hat{N} the operator associated with noise addition. Even for an ideal amplifier, this noise term must be added to ensure the preservation of the commutation relations $[\hat{a}_i, \hat{a}_i^\dagger] = 1$, and must satisfy $[\hat{N}, \hat{N}^\dagger] = (1 - G)$. Thus it can be divided in two parts: a fundamental quantum part given by $\hat{N}_q = \sqrt{G-1}\hat{a}_{int}^\dagger$, where \hat{a}_{int} is associated with the unavoidable fluctuations of the internal bosonic mode, and a scalar classical part denoted N_{cl} . Therefore a phase insensitive amplifier working at the quantum noise limit (i.e. $N_{cl} = 0$) obeys the relation [3]:

$$\hat{a}_{out} = \sqrt{G}\hat{a}_{in} + \sqrt{G-1}\hat{a}_{int}^\dagger \quad (1)$$

The intrinsic quantum noise, described by \hat{a}_{int} , can be traced back to different physical processes. For instance, spontaneous emission is unavoidably introduced in laser amplification, whereas, in parametric amplifiers and four wave mixers, vacuum fluctuations of the idler mode are added to the output signal [5, 6, 7]. In Raman amplifiers and Brillouin amplifiers zero-point fluctuations of respectively lattice vibrational modes (optical phonon) and acoustic phonon modes cause the noise [1].

The efficiency of a phase-insensitive amplifier is typically quantified by the noise figure [3, 9], which is defined by $NF \equiv \text{SNR}_{out}/\text{SNR}_{in}$. Here $\text{SNR}_{in(out)}$ is the signal-to-noise ratio of the input (output) field. For coherent state amplification, the noise figure then reads

$$NF = \frac{G}{2G - 1 + \Delta^2 N_{cl}} \quad (2)$$

which is maximized for quantum noise limit operation corresponding to $\Delta^2 N_{cl} = 0$. However, provided that the spurious technical noise N_{cl} is constant or has only a

weak dependence on G , the noise figure still approaches the quantum limit of 3dB in the high gain regime. The situation is different at low gains, as technical noise or internal losses become devastating for quantum noise limited performance [8, 9]. To date, these effects have hitherto prevented the full demonstration of quantum noise limited phase-insensitive amplification in the low gain regime [11], which is the domain of interest in the context of quantum information science.

For sake of completeness we mention that another class of amplifiers characterized by phase sensitive operation allows for noiseless amplification, provided the analysis is restricted to just one quadrature [3, 9]. Such an amplifier is described by the relation: $\hat{a}_{out} = (1 + G)/\sqrt{4G}\hat{a}_{in} + (1 - G)/\sqrt{4G}\hat{a}_{in}^\dagger$ and the noise figure is: NF=1.

We now show that the amplifier transformation (Eq. 1) can be realized using only linear optics, homodyne detection and feedforward, rendering the complex coupling between a strong pump and the signal inside a nonlinear crystal superfluous. Our scheme is illustrated schematically inside the dashed box in Fig. 1, and runs as follows. The input signal, represented by \hat{a}_{in} , is impinging on a beam splitter with transmission T and reflectivity R , and hence transformed into $\hat{a}'_{in} = \sqrt{T}\hat{a}_{in} - \sqrt{R}\hat{v}_1$ where the annihilation operator \hat{v}_1 represents the vacuum mode entering the dark port of the beam splitter. Conjugate quadrature amplitudes, e.g. the amplitude $\hat{x} = \hat{a} + \hat{a}^\dagger$ and the phase quadrature $\hat{p} = -i(\hat{a} - \hat{a}^\dagger)$, are simultaneously measured on the reflected part by dividing it on a 50/50 beam splitter and subsequently performing homodyne measurements on the two output beams. The measured quadratures are

$$\hat{x}_m = \frac{1}{\sqrt{2}}(\sqrt{R}\hat{x}_{in} + \sqrt{T}\hat{x}_{v1} + \hat{x}_{v2}) \quad (3)$$

$$\hat{p}_m = \frac{1}{\sqrt{2}}(\sqrt{R}\hat{p}_{in} + \sqrt{T}\hat{p}_{v1} - \hat{p}_{v2}) \quad (4)$$

Here $\hat{x}_{v(1,2)}$ and $\hat{p}_{v(1,2)}$ denote the quadratures of the uncorrelated vacuum modes entering at the two beam splitters. These projective measurements (with outcomes represented by their eigenstates and corresponding eigenvalues x_m and p_m) are then used to control a unitary displacement operation on the remaining system [12]. The feedforward loop can be described without any measurement by considering the unitary operator, $\hat{D} = \exp(g\hat{x}_m(\hat{a}_s - \hat{a}_s^\dagger))\exp(ig\hat{p}_m(\hat{a}_s + \hat{a}_s^\dagger))$, where g is the electronic gain and then subsequently tracing out the "measured" system. This results in the following transformation: $\hat{a}'_s \rightarrow \hat{D}^\dagger \hat{a}'_s \hat{D} = \hat{a}'_s + g(\hat{x}_m + i\hat{p}_m)/2$ and by choosing an electronic gain of $g = \sqrt{2R/T}$ we arrive at

$$\hat{a}_{out} = \sqrt{\frac{1}{T}}\hat{a}_{in} + \sqrt{\frac{1}{T} - 1}\hat{v}_2^\dagger \quad (5)$$

Setting $G = \frac{1}{T}$, we exactly recover the transformation for an ideal phase-insensitive amplifier given by (1), where

the amplification factor is controlled by the beam splitting ratio. Note that the noise that enters from the vacuum fluctuations on ν_1 is automatically cancelled out in the output via the feedforward. We also note that a related scheme, where noise entering a beam splitter was cancelled via feed forward, was used in ref. [13] to build a noiseless amplifier (with NF=1 for the amplitude quadrature). However, in contrast to our proposal, this scheme, apart from being phase sensitive, was not fully operating at the fundamental quantum limit [3]. A truly quantum noise limited phase sensitive amplifier based on the same principles was recently proposed [14], but it requires a nonclassical resource, namely a squeezed vacuum state.

Interestingly, the fundamental amplifier noise, represented by \hat{v}_2 , arises from the vacuum fluctuations that enter through the dark port of the 50/50 beam splitter used for \hat{x} and \hat{p} quadrature measurements. The amplifier noise is therefore directly related to the noise penalty associated with simultaneous measurement of conjugate quadratures. The close link between amplification and measurement theory [3] is thus particularly emphasized by our scheme.

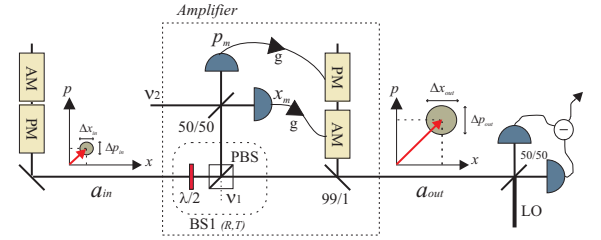


FIG. 1: *Conceptual diagram of the amplifier setup. The gain is determined by the transmission of the equivalent beam splitter (BS), (realized here by a combination of a half wave plate and a polarizing beam splitter (PBS)). AM and PM are amplitude and phase modulators respectively. Also shown are the phase space diagrams of the input coherent state and the amplified output state.*

The amplifier proposed in this Letter is phase-insensitive, and, in principle, amplifies any input state at the quantum limit. In the following, we demonstrate experimentally the amplification of a particular quantum state, namely the coherent state. The experimental setup is shown in Fig. 1. The laser source was a monolithic continuous wave Nd:YAG laser at 1064 nm. A small part of the laser beam was tapped off to serve as an input signal to the amplifier and the rest was used as local oscillator beams. Since the output from a laser is not a perfect coherent state due to low frequency technical noise, we define our coherent state to reside at a certain sideband frequency which we chose to be 14.3 MHz, within a bandwidth of 100kHz. At this frequency the laser was found to be shot noise limited, and by applying modulations at 14.3 MHz (by independently controlling an amplitude and a phase modulator), the sidebands are excited and

thus serve as a perfect coherent state.

The coherent state is then directed to the amplifier where it is divided by a beam splitter; the reflected part is measured and the transmitted part is displaced according to the measurement outcomes. Simultaneous measurements of the amplitude and phase quadrature are performed by combining the reflected signal beam with an auxiliary beam, ν_2 , with a $\pi/2$ phase shift and balanced intensities. The sum and difference of the photocurrents generated by two high quantum efficiency photodiodes then provide the simultaneous measurement of amplitude and phase quadrature (this strategy is not shown explicitly in the figure). The outcomes are sent to electronic amplifiers with appropriate gains and then finally fed into independent modulators. The modulators are placed in an auxiliary beam which is coupled to the signal beam via an asymmetric beam splitter which transmits 99% of the signal and reflects 1% of the auxiliary beam, thus leading to a negligible small noise addition. After displacement, the amplified signal is directed into a homodyne measurement system for verification.

The performance of the system is characterized by measuring the spectral noise properties of the signal before and after amplification. Since the quadrature statistics of the involved fields are Gaussian, measurements of the first ($\langle \hat{x}(\hat{p})_{out} \rangle$) and second moments ($\Delta^2 \hat{x}(\hat{p})_{out}$) of two conjugate observables, such as the amplitude and phase quadrature, suffice to fully characterize the states. Both quadratures are measured at the sideband frequency using a standard homodyne detection techniques. To ensure consistent comparison between the input and output signal, these measurements are realized by the same homodyne detector.

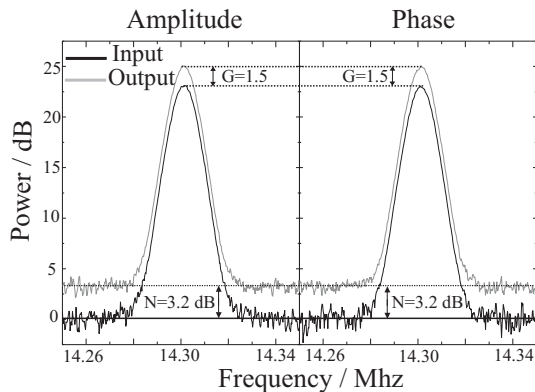


FIG. 2: Power spectra showing the operation of the amplifier for conjugate quadratures. The beam splitter was set to 1:2 enabling an optical gain of $G = 1.5$ (1.8dB). The mean value of the field is amplified by 1.8dB and the noise is consequently increased by 3.2dB, which is very close to the ideal noise level of 3dB above the shot noise. The noise figure is $NF = 0.7$. The resolution bandwidth is 10kHz and the video bandwidth is 30Hz.

An example of a specific amplifier run is shown in Fig. 2. Here we set the beam splitting ratio to 1:2 in order to reach an optical gain of 1.5. The spectral densities of the amplitude and phase are shown over a 100 kHz frequency span for the input signal and the amplified output signal. Considering the whole span as a part of the quantum state, the heights of the peaks correspond to the coherent mean values whereas the noise floor can be regarded as the actual noise in the state. Therefore the amplification factor, which is roughly the difference between the input and output peaks, as well as the added noise, which is the difference between the shot noise limit and the noise floor, can be easily estimated. It is evident from the plots that additional noise has been added to the signal as a result of the amplification process.

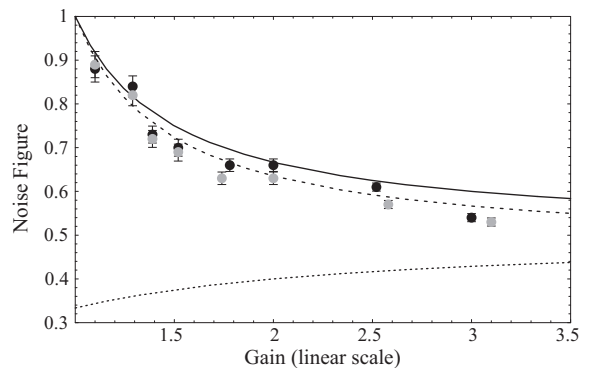


FIG. 3: The noise figure, NF , as a function of the gain, G . The black (grey) dots represent the experimental data for the amplitude (phase) quadrature. The solid line represent the quantum noise limit (given by Eq. 2), whereas the predicted noise figure for our device with imperfect detectors is shown by the dashed line. For comparison, the dotted line corresponds to an amplifier with two vacuum units of extra technical noise. Errors mainly stem from the inaccuracy in determining the quantum efficiency of the photodiodes.

To evaluate the noise figure, we estimated accurately the gain and the added noise at 14.3 MHz. This was realized in a zero span measurement over 2 seconds by subsequently switching on and off the modulation. Moreover, to avoid erroneously underestimation of the noise power, all the measurement have been corrected for losses occurring in the homodyne detection. The total efficiency, including mode matching and photodiode quantum efficiency, has been carefully estimated to $\eta_{hd} = 0.83$.

In Fig.3, we report the noise figure of our amplifier for a whole range of gains (corresponding to different transmission coefficients and optimized electronic gains). By comparing the experimental results with the ideal ones (calculated from Eq.(2) and indicated by the solid line), we clearly see that the amplifier operates close to the fundamental limit even for low amplification factors. The small deviation to the ideal amplifier performance is due to imperfections in the in-line homodyne detector and feed-forward electronics. These limiting factors were partly

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